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European Technical Assessment ETA-23/1017 of 2024/03/26

I General Part

Technical Assessment Body issuing the ETA and designated according to Article 29 of the Regulation (EU) No 305/2011: ETA-Danmark A/S

Trade name of the construction product:	Wimmer post bases type ISB, Nippel, Uni and Variomax
Product family to which the above construction product belongs:	Three-dimensional nailing plate (Post bases)
Manufacturer:	Stefan Wimmer GmbH Hitzendorferstraße 13 A-8561 Söding - St. Johann Tel. +43 3142 22025-0 Fax + 43 3142 22025-50 Internet www.holzbau-shop.at
Manufacturing plant:	Herstellerwerk 1
This European Technical Assessment contains:	29 pages including 3 annexes which form an integral part of the document
This European Technical Assessment is issued in accordance with Regulation (EU) No 305/2011, on the basis of:	EAD 130186-00-0603 for Three-dimensional nailing plates
This version replaces:	

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II SPECIFIC PART OF THE EUROPEAN TECHNICAL ASSESSMENT

1 Technical description of product

The post bases are made of steel plates in combination with steel tubes or threaded rods and are available in various types and sizes. The post bases are produced of steel grade S235 according to EN 10025-2. The steel tubes and rods are produced from steel grade S235 according to EN 10277-2 and the threaded rods correspond to property class 4.8 according to EN ISO 898-1. The zinc nickel coating – applied as a corrosion protection – is defined as Fe//ZnNi10//Cn//T2, with a minimum thickness of 10 μ m and a nickel content of 10 to 15 M.-%.

For the connections with metal fasteners according to ETA-17/0803 or ETA-12/0471 are used. The screws shall be driven into pre-drilled holes according to EN 1995-1-1, 10.4.5 or respectively according to the ETA of the screws.

Dimensions are shown in Annex A and B.

2 Specification of the intended use in accordance with the applicable European Assessment Document (hereinafter EAD)

The intended use of the post bases is the support of timber columns and posts as load-bearing elements, where requirements for mechanical resistance and stability and safety in use in the sense of the Basic Works Requirements 1 and 4 of Regulation (EU) 305/2011 shall be fulfilled.

The static and kinematical behaviour of the timber members or the supports shall be as described in Annex B.

The timber posts may be of solid timber of strength class C24 or better according to EN 338:2016 or of glued laminated timber according to EN 14080:2013. Minimum dimensions for the post have to be considered (Annex A).

The post base shall be installed as pictured in the drawings. The cross-section of the timber column shall

be positioned centrically and with the end grain plane on the base plate. The end grain of the timber post must in general be plane on the base plate of the post base. Post bases types H have a distance between the end grain of the timber post and the base plate of the post base up to 10 mm due to constructive wood preservation.

The maximum distance between the foundation and the base plate of the post base is given in Annex A, table A.1.

Annex B states the load-carrying capacities of the post bases for solid timber of strength class C24 according to EN 338:2016. The design of the connections shall be in accordance with Eurocode 3 and Eurocode 5 or a similar national code. The anchorage of the post base in the foundation and imperfections exceeding the assumptions in Eurocode 5, 5.4.4 are not part of this ETA.

The post bases are for use in timber structures subject to the service classes 1, 2 and 3 of Eurocode 5 and for connections subject to static or quasi-static loading. The corrosion protection is given by zinc nickel coating – applied as a corrosion protection – is defined as Fe//ZnNi10//Cn//T2, with a minimum thickness of 10 μ m and a nickel content of 10 to 15 M.-%.

The metal fasteners must also have a zinc coating according to EN ISO 2081 corresponding to the relevant service class 1, 2 or 3 of EN 1995-1-1. Galvanic zinc coating of the post bases is only suitable for service classes 1 and 2.

The scope of the hangers regarding resistance to corrosion shall be defined according to national provisions that apply at the installation site considering environmental conditions.

The provisions made in this European Technical Assessment are based on an assumed intended working life of the post bases of 50 years.

The indications given on the working life cannot be interpreted as a guarantee given by the producer or Assessment Body, but are to be regarded only as a means for choosing the right products in relation to the expected economically reasonable working life of the works.

Chara	acteristic	Assessment of characteristic		
3.1	Mechanical resistance and stability*) (BWR1)			
Joint S	Strength - Characteristic load-carrying capacity	See Annex B		
Joint Stiffness		No performance assessed		
Joint ductility		No performance assessed		
Resistance to seismic actions		No performance assessed		
Resistance to corrosion and deterioration		See section 3.6		
3.2	Safety in case of fire (BWR2)			
	Reaction to fire	The post bases are made from steel classified as Euroclass A1 in accordance with EN 13501-1 and Commission Delegated Regulation 2016/364		
	Resistance to fire	No performance assessed		
3.3	General aspects related to the performance of the product	The angle brackets have been assessed as having satisfactory durability and serviceability when used in timber structures using the timber species described in Eurocode 5 and subject to the conditions defined by service class 1, 2 and 3		
	Identification	See Annex A		
	dditional information in section 3.4 3.6			

3 Performance of the product and references to the methods used for its assessment

*) See additional information in section 3.4 - 3.6.

3.4 Mechanical resistance and stability

Safety principles and partial factors

The characteristic load-carrying capacities are based on the characteristic values of the connections with metal fasteners, the steel components and the timber post.

In the case of timber failure or failure of the metal fasteners, the design values shall be calculated according to EN 1995-1-1 by dividing the characteristic values of the load-carrying capacities by different partial factors for the strength properties, and in addition multiplied with the coefficient k_{mod} .

In the case of steel failure, the design value shall be calculated according to EN 1993-1-1 by reducing the characteristic values of the load-carrying capacity with different partial factors.

The design value of the load-carrying capacity is the smaller value of all load-carrying capacities:

$$F_{Rd} = \min\left\{\frac{k_{mod} \cdot F_{Rk,T}}{\gamma_{M,T}}; \frac{F_{Rk,S}}{\gamma_{Mi,S}}\right\}$$

Therefore, for timber failure or failure of the metal fasteners the load duration class and the service class are included. The different partial factors γ_M for steel or timber failure, respectively, are also correctly taken into account

Mechanical resistance and stability

See Annex B for the characteristic load-carrying capacity in the different directions F_1 to F_5 for solid timber of strength class C24 according to EN 338. Using the load-carrying capacities of the post bases, the specifications in Annex A must be fulfilled.

The characteristic capacities of the post bases are determined by a combination of calculation according to Eurocode 3 and Eurocode 5 and testing. They should be used for designs in accordance with Eurocode 3 and Eurocode 5 or a similar national code.

No performance has been determined in relation to ductility of a joint under cyclic testing. The contribution to the performance of structures in seismic zones, therefore, has not been assessed.

No performance has been determined in relation to the joint's stiffness properties - to be used for the analysis of the serviceability limit state.

No performance has been determined in relation to the anchorage of the post bases in the foundation. It must be checked by the designer of the structure to ensure it is not less than the post base capacity and, if necessary, the post base capacity reduced accordingly. Therefore the specifications for the lever arms $e_{F2/F3}$ (for load case F_2 / F_3) and $e_{F4/F5}$ (for load case F_4 / F_5) in annex A have to be considered. The lever arm is the distance between the top edge of the foundation and the load.

3.5 Aspects related to the performance of the product

2.7.1 Corrosion protection in service class 1 and 2. In accordance with EAD 130186-00-0603 the post bases are produced from steel grade S235 according to EN 10025-2 with a minimum characteristic yield strength of $R_{eH} = 235$ N/mm² and a minimum characteristic tensile strength of $R_m = 360$ N/mm² The steel tubes and rods are produced from steel grade S235 according to EN 10277-2 and the threaded rods correspond to property class 4.8 according to EN ISO 898-1.

The post bases are for use in timber structures subject to the service classes 1, 2 and 3 of Eurocode 5 and for connections subject to static or quasi-static loading. The zinc nickel coating – applied as a corrosion protection – is defined as Fe//ZnNi10//Cn//T2, with a minimum thickness of 10 μ m and a nickel content of 10 to 15 M.-%.

The metal fasteners must also have a zinc coating according to EN ISO 2081 corresponding to the relevant service class 1, 2 or 3 of EN 1995-1-1.

3.6 General aspects related to the fitness for use of the product

The performances given in this ETA are based on the following:

- The timber post
 - shall be restrained against rotation, and supported at the lower and upper end
 - shall be strength class C24 or better according to EN 338
 - shall be free from wane in the post base
 - must fulfil the requirements regarding minimum dimensions (see Annex A)
 - end grain must in general be plane on the base plate or spacer of the post base or at a maximum distance given in Annex A.
- The post base shall be installed centrically in the cross-section of the timber column.
- The actual end bearing capacity of the timber member to be used in conjunction with the post base is checked by the designer of the structure to

ensure it is not less than the post base capacity and, if necessary, the post base capacity reduced accordingly.

- There are no specific requirements relating to preparation of the timber members.
- The minimum insertion depth in the turnbuckles should be the diameter of the rod.
- The base plates of the post bases with steel tubes as support must in general be plane on the tube's end.
- The anchorage of the post base in the foundation is not part of this ETA. It must be checked by the designer of the structure to ensure it is not less than the post base capacity and, if necessary, the post base capacity reduced accordingly. Therefore, the specifications for the lever arms $e_{F2/F3}$ (for load case F_2 / F_3) and $e_{F4/F5}$ (for load case F_4 / F_5) in Annex A have to be considered. The lever arm is the distance between the top edge of the foundation and the load.

4 Assessment and verification of constancy of performance (hereinafter AVCP) system applied, with reference to its legal base

4.1 AVCP system

According to the decision 97/638/EC of the European Commission1, as amended, the system(s) of assessment and verification of constancy of performance (see Annex V to Regulation (EU) No 305/2011) is 2+.

5 Technical details necessary for the implementation of the AVCP system, as provided for in the applicable EAD

Technical details necessary for the implementation of the AVCP system are laid down in the control plan deposited at ETA-Danmark prior to CE marking.

Issued in Copenhagen on 2024-03-26 by

Thomas Bruun Managing Director, ETA-Danmark

Page 8 of 29 of European Technical Assessment no. ETA-23/1017, issued on 2024-03-26 Annex A Product details and definitions

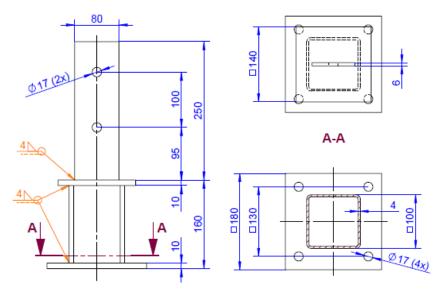
Type "ISB"

The post base type "ISB" consists of a rectangular-shaped steel tube (100 x 100 mm, t = 4 mm) with varying length l_{tube} ("ISB 160": $l_{tube} = 140$ mm; "ISB 260": $l_{tube} = 240$ mm) and a welded steel plate with 140 x 140 x 10 mm (top) and one with 180 x 180 x 10 mm (bottom) on each end. Thereby, the top plate serves as contact surface to the timber member's end grain. It consists of a steel slot with t = 6 mm and a length x width of 250 x 80 mm and two boreholes with d = 17 mm, wherein two dowels or bolts can be placed as parts of a steel-to-timber shear connection (two shear planes). With the bottom plate, the post base is connected with the basement. Therefore, four boreholes with d = 17 mm, each close to each corner, are designated.

In table A.1 the main geometrical properties of both considered types are given, the related drawing is shown exemplarily for type ISB 160 in figure A.1.

type		geom	ietry			
	bottom plate	top plate	steel tube	steel slot	no. and diameter of dowels/bolts	
	<i>l / w / t</i> [mm]	l / w / t [mm]	<i>l</i> _{tube} / <i>w</i> / <i>t</i> [mm]	<i>l / w / t</i> [mm]		
ISB 160	190 / 190 / 10	140 / 140 /	140 / 100 / 4	250 / 80 / 6	$2 \mid d = 17 \text{ mm}$	
ISB 260	180 / 180 / 10	10	240 / 100 / 4	250 / 80 / 6	$2 \mid a = 17$ mm	

Table 1: Denotation and dimensions of the relevant components of the post base types "ISB"



Firgure A.1: Drawings of the post base type "ISB 160" (dimensions in [mm])

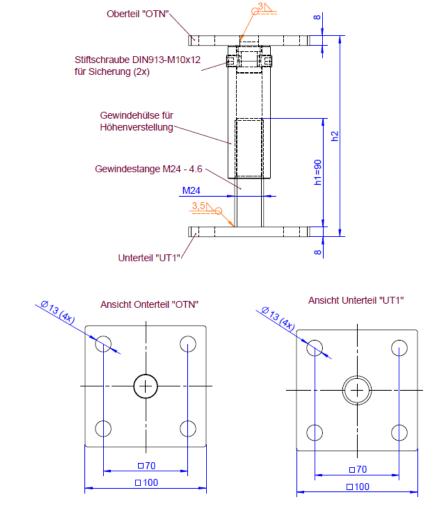
Type "Nippel"

The post base type "Nippel" has a varying height $h_2 = 131 \div 421$ mm. This is realized by threaded rods M24 with varying length h_1 (type "UT 1" and "UT 2": $h_1 = 90$ mm, type "UT 3": $h_1 = 250$ mm, type "UT 4": $h_1 = 330$ mm) in combination with an adjustable screwed connection between the threaded rod M24 and a circular-shaped steel tube and an inner thread, fitting to the one of the threaded rod. The latter is welded on a steel (bottom) plate with either 100 x 100 x 8 mm (type "UT 1") or 100 x 160 x 8 mm (types "UT 2", "UT 3" or "UT 4"). Both plate geometries consist of four boreholes with d = 13 mm, which are closely located to plate's corners and serve for the connection of the post base with the basement. On its other, unthreaded end the steel tube consists of two boreholes, which are oriented perpendicular to its axis and in which two stud bolts M10 x 12 mm can be anchored. These stud bolts connect the steel tube with a fitting (in German "Nippel"), which is welded on a steel plate with 100 x 100 x 8 mm ("OTN"). This top plate serves as contact surface to the timber member's end grain. Identical to the bottom plate it consists of four boreholes with d = 13 mm, which are closely located self-tapping timber screws with a washer head and $d / l_{screw} = 10 / 100$ mm; according to ETA-17/0803.

In tabale A.2**Fejl! Henvisningskilde ikke fundet.** the main geometrical properties of the subtypes "UT 1" to "UT 4" are given, the related drawings are shown in figure A.2, exemplarily for type "UT 1".

		no. and				
subtype	height adjustment h_2	nt h_2 bottom plate top plate		threaded rod	diameter of	
	[mm]	<i>l / w / t</i> [mm]	l / w / t [mm]	<i>h</i> ₁ / <i>d</i> [mm]	self-tapping screws	
UT 1	131 ÷ 181	100 / 100 / 8		90 / M24		
UT 2	131 ÷ 181	160 / 100 / 8	100 / 100 / 9	90 / M24	4 1 10	
UT 3	291 ÷ 341	160 / 100 / 8	100 / 100 / 8	250 / M24	$4 \mid d = 10 \text{ mm}$	
UT 4	371 ÷ 421	160 / 100 / 8		330 / M24		

Table A.2:
"Nippel"Denotation and dimensions of the relevant components of the post base types



Page 10 of 29 of European Technical Assessment no. ETA-23/1017, issued on 2024-03-26

Figure A.2: Drawings of the post base type "Nippel" (dimensions in [mm])

Type "UNI"

The post base type "UNI" has a varying height $h_2 = 59 \div 338$ mm. This is realized by threaded rods M24 with varying length h_1 (type "UT 1" and "UT 2": $h_1 = 90$ mm, type "UT 3": $h_1 = 250$ mm, type "UT 4": $h_1 = 330$ mm) and welded on a steel (bottom) plate with either 100 x 100 x 8 mm (type "UT 1") or 100 x 160 x 8 mm (types "UT 2", "UT 3" or "UT 4") in combination with two different types of steel top plates (both 100 x 100 x 8 mm), denoted as "OTM" and "OTW". The type "OTM" has a centrically situated hole with circular shape and a nut M24, which is welded on the steel plate. The height adjustment is enabled by screwing the threaded rod through the nut and the hole. In case of type "OTW", the nut is replaced by a hook-shaped steel angle (in German "Sicherungswinkel") with a circular hole (d = 26 mm). Thereby the height adjustment / installation is enabled by merging the threaded rods through the steel angle's and the top plate's holes, whereby two nuts M24, one below the steel angle and one between the steel plates to connect with the basement and the timber member is identical to the post base type "Nippel", see above.

		geometry						
subtype	top plate type	height adjustment h ₂	bottom plate	top plate	threaded rod	diameter of self- tapping		
		[mm]	<i>l / w / t</i> [mm]	<i>l / w / t</i> [mm]	$h_1 / d \text{ [mm]}$	screws		
UT 1	OTM	59 ÷ 98	100 / 100 / 8		90 / M24			
011	OTW	63 ÷ 98	160 / 100 / 8 160 / 100 / 8 160 / 100 / 8	100 / 100 / 8		90714		
UT 2	OTM	59 ÷ 98		100 / 100 / 9	90 / M24	4 d =		
012	OTW	63 ÷ 98						
	OTM	219 ÷ 258		100/100/8	250 / M24	10 mm		
UT 3	OTW	223 ÷ 258			2307 WI24			
UT 4	OTM	299 ÷ 338	160 / 100 / 8		330 / M24			
014	OTW	303 ÷ 338	160 / 100 / 8		3307 W124			

In table A.3 the main geometrical properties of the subtypes "UT 1" to "UT 4" and "OTM" vs. "OTW" respectively are given, the related drawings are shown in figure A.3, exemplarily for type "UT 1".

Table A.3:
"UNI"Denotation and dimensions of the relevant components of the post base types

Page 12 of 29 of European Technical Assessment no. ETA-23/1017, issued on 2024-03-26

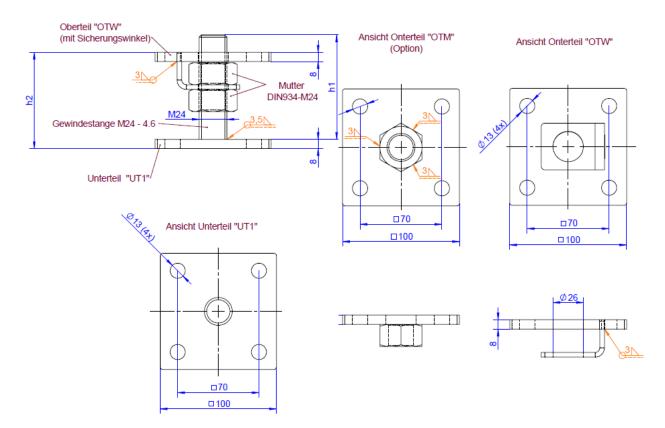


Figure A.3: Drawings of the post base type "UNI" (dimensions in [mm])

Type "Variomax"

The post base type "Variomax" has a varying height $h_2 = 140 \div 437$ mm. This is realized by threaded rods M24 or M30 with varying lengths h_1 (M24: type "UT 2": $h_1 = 90$ mm, type "UT 3": $h_1 = 250$ mm, type "UT 4": $h_1 = 330$ mm | M30: type "UT 5": $h_1 = 90$ mm, type "UT 6": $h_1 = 250$ mm) and welded on a steel (bottom) plate with 100 x 160 x 8 mm (identical for all types "UT 2" top "UT 6") in combination with a circular-shaped steel tube with inner threads, fitting to the ones of the threaded rods. The connection between the steel tube with the steel top plate, given either with a quadratic (100 x 100 x 8 mm, denoted as "OTV") or a circular shape (d = 120 mm, denoted as "OTV-Rund") is realized via a centrically positioned stud bolt, which is welded on the steel top plate and connected with the steel tube via a union nut. This enables a separate assembly of the top plate on the timber member and of the bottom plate on the basement. While the latter is equal to types "Nippel" and "UNI", for the connection to the timber member n = 4 (quadratic) vs. 3 (circular) inclined (15 ° vs. 10 °) countersunk drillings for d = 8 mm fully threaded self-tapping timber screws with $l_{screw} = 160$ mm according to ETA-12/0471 are given.

In table A.4 the main geometrical properties of the subtypes "UT 2" to "UT 6" and "OTV" vs. "OTV-Rund" respectively are given, the related drawings are shown in figure A.4, exemplarily for type "UT 2 / UT 3 / UT 4".

			geometry						
subtype	top plate type	height adjustment h ₂	bottom plate	top plate	threaded rod	no. and diameter of self-tapping			
		[mm]	<i>l / w / t</i> [mm]	<i>l / w / t</i> or <i>d / t</i> [mm]	h_1 / d [mm]	screws			
UT 2	OTV	140 ÷ 190		100 / 100 / 8	90 / M24	$4 \mid d = 8 \text{ mm}$			
012	OTV-Rund	147 ÷ 197		120 / 8	90711124	$3 \mid d = 8 \text{ mm}$			
	OTV	300 ÷ 350		100 / 100 / 8	250 /	$4 \mid d = 8 \text{ mm}$			
UT 3	OTV-Rund	307 ÷ 357		120 / 8	M24	$3 \mid d = 8 \text{ mm}$			
	OTV	380 ÷ 430	160/100/9	100 / 100 / 8	330 /	$4 \mid d = 8 \text{ mm}$			
UT 4	OTV-Rund	387 ÷ 437	160 / 100 / 8	120 / 8	M24	$3 \mid d = 8 \text{ mm}$			
	OTV	142 ÷ 192		100 / 100 / 8	00 / 11/20	$4 \mid d = 8 \text{ mm}$			
UT 5	OTV-Rund	149 ÷ 199		120 / 8	90 / M30	$3 \mid d = 8 \text{ mm}$			
	OTV	302 ÷ 352		100 / 100 / 8	250 /	$4 \mid d = 8 \text{ mm}$			
UT 6	OTV-Rund	309 ÷ 359		120 / 8	M30	$3 \mid d = 8 \text{ mm}$			

Tabke A.4:Denotation and dimensions of the relevant components of the post base types"Variomax"

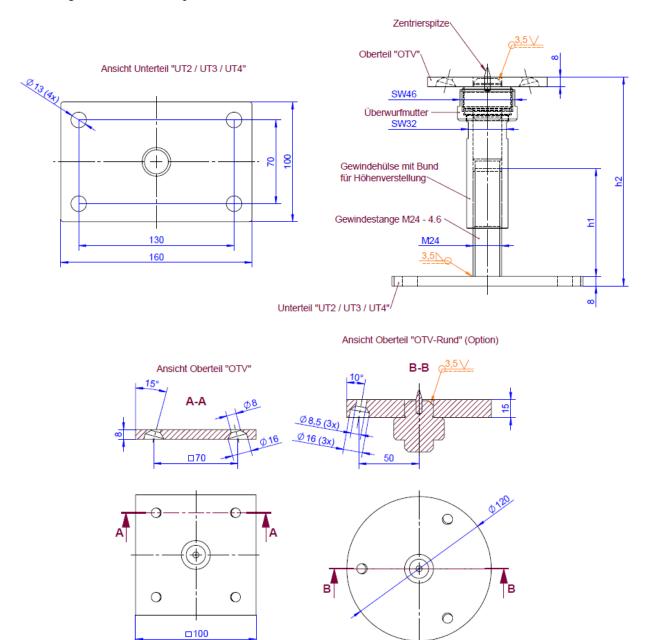


Figure A.4: Drawings of the post base type "Variomax" (dimensions in [mm])

Annex B Characteristic load-carrying capacities

Characteristic load-carrying capacities of post base type "ISB" in dependence of the load type and direction F_i

			failure mode						
load type and direction		timber/co	onnection	steel					
		member (stress)	connection	member (stress)	connection	buckling			
		$k_{ m mod}/\gamma_{ m M}$	$k_{ m mod}/\gamma_{ m M,C}$	γм,0	γм,2	γ _{M,1}			
			[kN]	[kN]	[kN]	[kN]			
$F_{1,c,k}$	compression	292* ÷ 402*	-	350	-	-			
$F_{1,t,k}$	tension	-	38.7**	-	122	-			
F _{2/3,k}	transversal	-	3.22	-	12.4	-			
F _{4/5,k}	transversal	-	7.01	1.35	-	-			
* value dene	nds on And can be	adjusted by f	$\sim 1/21$ in case	of a strength c	lass different t	0C24			

* value depends on A_{net} ; can be adjusted by $f_{c,0,k}$ / 21 in case of a strength class different to C24 ** can be adjusted according to ON EN 1995-1-1, Sections 8.2.3, 8.5 and 8.6 in case of strength classes differing from C24 and S235 respectively

Characteristic load-carrying capacities of post base type "Nippel" in dependence of the load type and direction F_i

			failure mode						
load type and direction		timber/co	onnection	steel					
		member (stress)	connection		connection	buckling			
		$k_{ m mod}/\gamma_{ m M}$	$k_{ m mod}/\gamma_{ m M,C}$	$\gamma_{M,0} / \gamma_{M,2}$	γм,2	γм,1			
			[kN]	[kN]	[kN]	[kN]			
$F_{1,c,k}$	compression	199*	-	-	-	87.5			
$F_{1,t,k}$	tension	-	17.0	-	-	-			
$\begin{array}{c c} F_{2/3,k} \& \\ F_{4/5,k} \end{array} transversal \\ \end{array}$		-	-	-	1.50	-			
* value can b	be adjusted by $f_{c,0,k}$	/ 21 in case of	a strength class	ss different to (C24				

	load type and direction		failure mode					
			timber/co	onnection	steel			
type			member (stress)	connection	member (stress)	connection	buckling	
				$k_{\rm mod}/\gamma_{\rm M,C}$	$\gamma_{M,0} / \gamma_{M,2}$	γм,2	γм,1	
			[kN]	[kN]	[kN]	[kN]	[kN]	
OTM	F	compression	189*	-	-	-	99.8	
OTW	$F_{1,c,k}$	compression	189*	-	-	-	82.0	
OTM	E.	tension	-	17.0	-	-	-	
OTW	$F_{1,\mathrm{t},\mathrm{k}}$	tension	-	7.79	-	-	-	
OTM	$F_{2/3,k}$ &	transversal	-	-	1.74	-	-	
OTW	$F_{4/5,k}$	u ans ver sar	-	-	-	-	-	
* value can	be adjusted	by $f_{c,0,k} / 21$ in c	ase of a strer	ngth class dif	ferent to C24	ļ		

Characteristic load-carrying capacities of post base type "Uni" in dependence of the load type and direction F_i

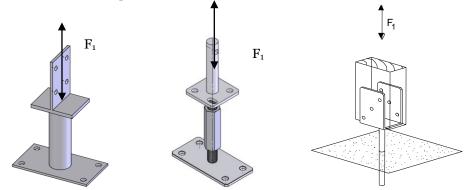
Characteristic load-carrying capacities of post base type "Variomax M24 / M30" in dependence of the load type and direction F_i

			failure mode					
				onnection	steel			
type	type load type and direction		member (stress)	connection	member (stress)	connection	buckling	
			$k_{ m mod}/\gamma_{ m M}$	$k_{ m mod}/\gamma_{ m M,C}$	$\gamma_{M,0} / \gamma_{M,2}$	γ _{М,2}	γ _{M,1}	
			[kN]	[kN]	[kN]	[kN]	[kN]	
OTV			206*	-	-	-	81.1 / 171	
OTV-	$F_{1,c,k}$	compression	234*	_	_	_	81.1 / 171	
Rund			234	_		_	01.17171	
OTV			-	33.0	-	-	-	
OTV-	$F_{1,\mathrm{t},\mathrm{k}}$	tension	_	27.6	_	_	_	
Rund				27.0	_			
OTV	$F_{2/3,k} \& F_{4/5,k}$		-	-	1.74 / 3.21	-	-	
OTV-		transversal	_	-	1.80 / 1.93	_	_	
Rund	1 4/J,K		_	_	1.00 / 1.75	_	-	
* value can	be adjusted	by $f_{c,0,k}$ / 21 in c	ase of a strer	ngth class dif	ferent to C24	Ļ		

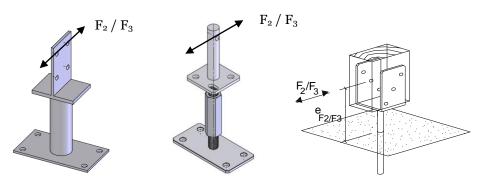
 $\gamma_{M(T)}$: partial factor for solid timber according to EN 1995-1-1 and national annex $\gamma_{M(C)}$: partial factor for connections according to EN 1995-1-1 and national annex $\gamma_{M,0;}\gamma_{M,1;}\gamma_{M,2}$: partial factors according to EN 1993-1-1 and national annex

Definitions of forces, their directions and eccentricity

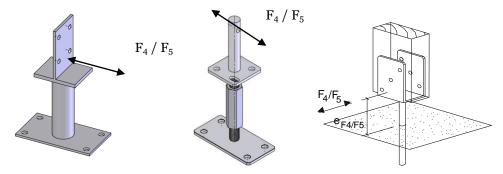
• Force F₁: tensile or compression load



- Force F_2 / F_3 : horizontal parallel to the ground plate of the post base and perpendicular to the bolts or dowels



• Force F_4 / F_5 : horizontal load parallel to the ground plate of the post base and parallel to the bolts or dowels



Acting forces

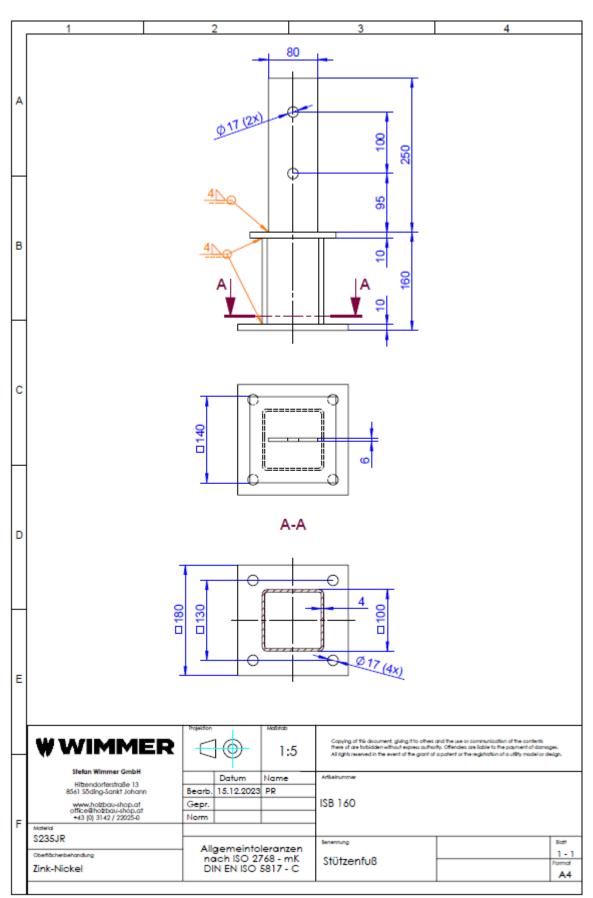
- F₁ axial force (tension or compression) acting along the central axis of the joint
- F_2 and F_3 horizontal force perpendicular to the ground plate of the post base acting with the lever arm $e_{F2/F3}$ above the foundation
- F_4 and F_5 horizontal force parallel to the ground plate of the post base acting with the lever arm $e_{F4/F5}$ above the foundation

Combined forces

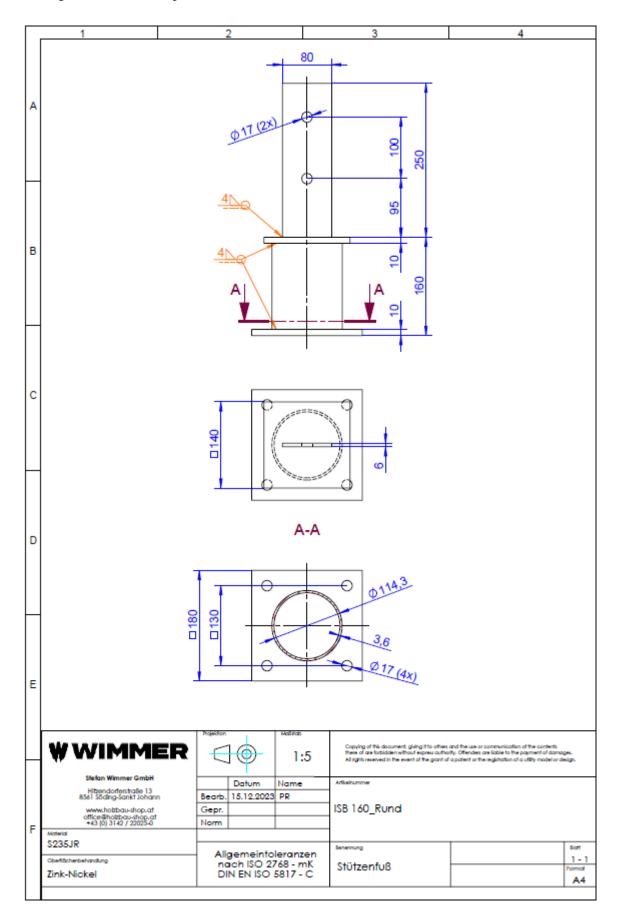
If the forces F_1 and F_2/F_3 or F_4/F_5 act at the same time, the following inequality shall be fulfilled:

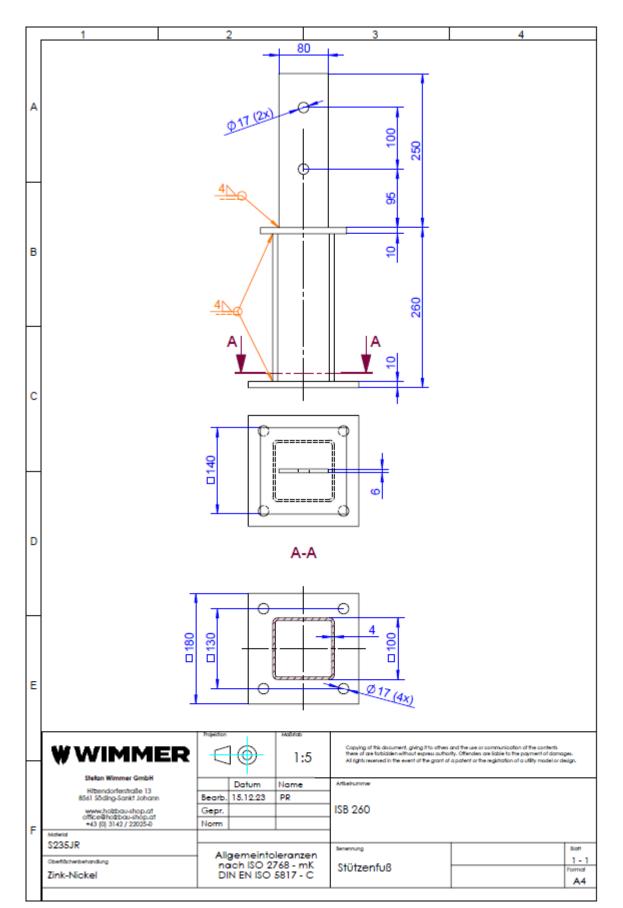
$$\sum \frac{F_{i,\text{Ed}}}{F_{i,\text{Rd}}} \leq 1$$

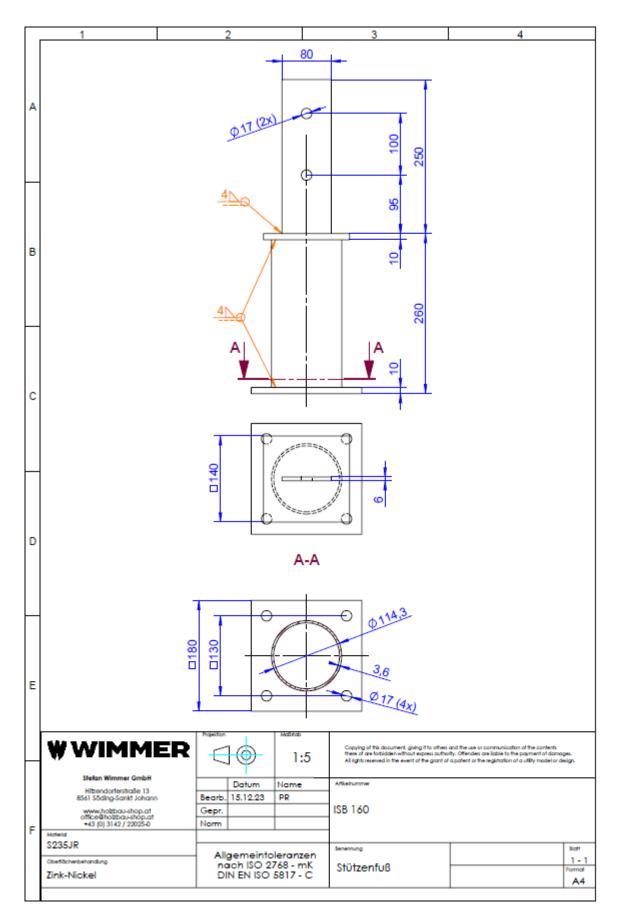
The forces F_2 and F_3 or F_4 and F_5 are forces with opposite direction. Therefore only one force F_2 or F_3 , and F_4 or F_5 , respectively, is able to act simultaneously with F_1 .

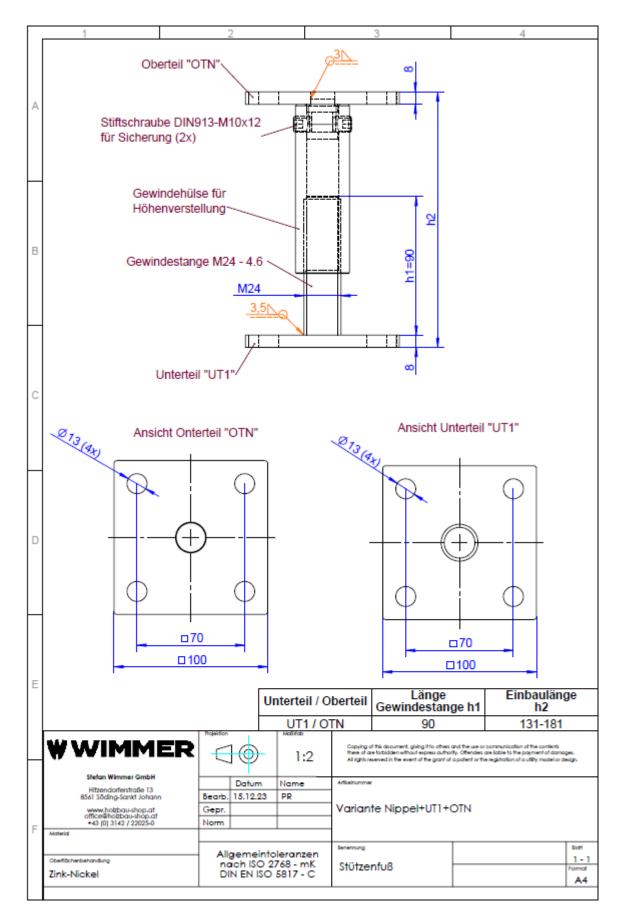


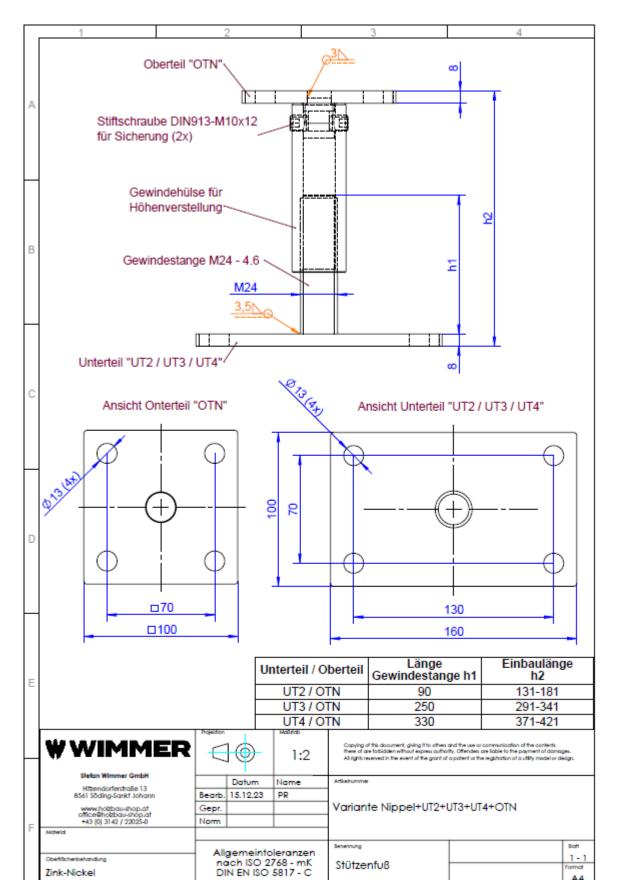
Annex C Product drawings







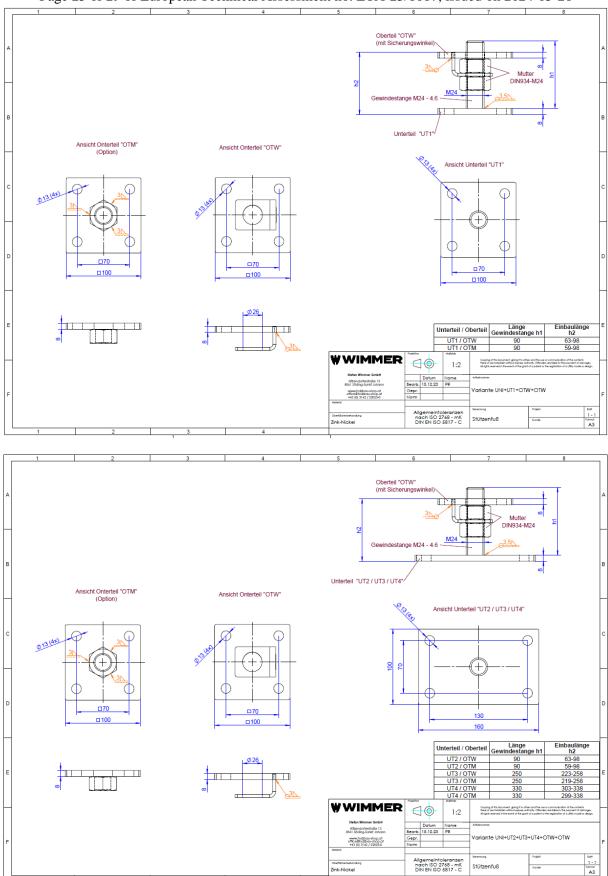




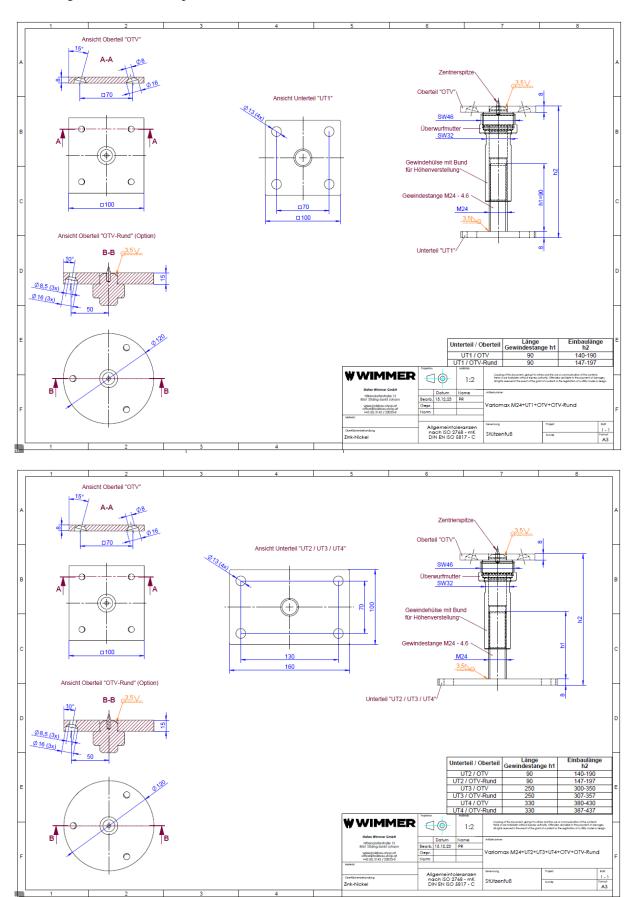
Stützenfuß

A4

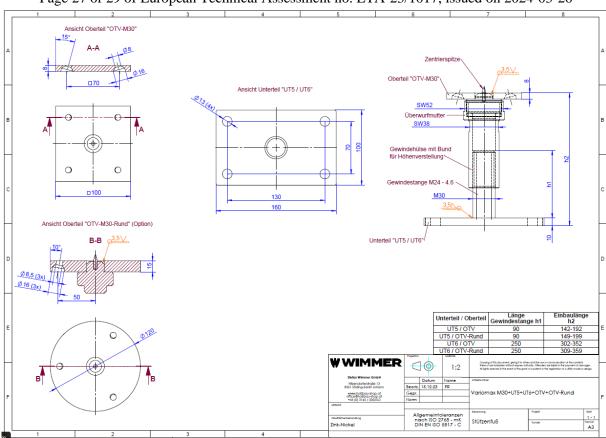
Zink-Nickel



Page 25 of 29 of European Technical Assessment no. ETA-23/1017, issued on 2024-03-26



Page 26 of 29 of European Technical Assessment no. ETA-23/1017, issued on 2024-03-26



Page 27 of 29 of European Technical Assessment no. ETA-23/1017, issued on 2024-03-26

